# Speeds of Sound and Excess Volumetric Properties of Mixtures of Water with 2-Propanol and with Ethylene Glycol Monoisopropyl Ether at 298.15 K

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Ultrasonic speeds of binary mixtures of water with 2-propanol and with ethylene glycol monoisopropyl ether have been measured at 298.15 K over the entire composition range. Density values were taken from the literature and combined with the measured values of the ultrasonic speeds to furnish estimates of the quantities  $-(\partial V/\partial p)_s$ , their excess counterparts, and the deviations of the ultrasonic speeds from the values calculated for ideal mixtures. The results have been analyzed using a segmented-composition model and compared with those previously obtained for related binary aqueous systems.

## Introduction

Our interest lies in exploring the extent to which the composition dependence of a variety of excess thermodynamic properties of nonionic amphiphile + water systems provides evidence for the existence of ordered patterns of molecular aggregation. In earlier papers, we have reported the results of our measurements of some thermodynamic properties of the aqueous mixtures of the family of poly-(ethylene glycol) monoalkyl ethers, whose members possess the generic formula  $C_m H_{2m+1}(OC_2 H_4)_n OH(C_m E_n)$  (1-3). These investigations were concerned with the sensitivity to the alkyl chain length of the composition dependence of the concerned excess molar properties, together with the deviations of the ultrasonic speed from a quantity assumed to represent its value in an ideal mixture. Our intention is to extend the field of our investigations to other types of structural modifications, namely, the branching in the alkyl group for isomeric species and the changes in the polar head. Our attention has been drawn to the interesting aspects of the composition dependence of the excess molar volumes of the aqueous solutions of two couples of model isomeric species, 1-propanol (4) and 2-propanol (5) on the one hand, 2-proposyethanol (6) and ethylene glycol monoisopropyl ether (7) on the other. Therefore, we thought it worthwhile to perform measurements of the ultrasonic speed of the 2-propanol + water and ethylene glycol monoisopropyl ether + water systems. There have been several investigations of ultrasonic speeds for the former system, but imprecision of measurements or sparseness of the results seemed to warrant a more detailed investigation of the mole fraction dependence of the compressibilities (8,**9**).

#### **Experimental Section**

Apparatus and Procedures. The speeds of sound, u, in both the pure liquids and their mixtures were measured

at 298.15 K, using the sing-around technique which involves the passing of successive pulses of 1.8 MHz acoustic waves through the solution cell, with the arrival of one pulse triggering the transmission of the next (10). The ultrasonic-pulse repetition rate (frequency f) was obtained by means of a sonic solution monitor (Mapco Inc., Nusonics Model 6105) and determined by a time-counter Hewlett-Packard 5384A. That rate is related to the speed of sound by a known explicit function of temperature and composition. The electronic processing circuit was coupled with a solution cell which is an 8 cm long brass cylinder (designed by E. Høgseth, Department of Chemistry, University of Bergen, Norway). The cell was submerged in an ultrathermostat, Heto 04 PE 623, which was provided with an auxiliary cooling device, Heto CB7. The temperature was controlled to within  $\pm 0.002$  K and measured with a Hewlett-Packard calibrated quartz thermometer of type 2804A. Measurements of the frequency f were performed 20 min after the cell was dipped into the water bath and repeated 10 min later. Each sample measurement was bracketed by two water measurements, since water was used as a calibrant to determine the ultrasonic speed of the samples. It is appropriate to note that the errors in the measured ultrasonic speeds have been demonstrated to depend upon the difference between those values and that of the reference fluid (11). The maximal error of the speeds measured relative to water [1496.687  $\text{m}\cdot\text{s}^{-1}$  at 298.15 K (12)] is believed to be less than  $0.2 \text{ m}\cdot\text{s}^{-1}$ ; the reproducibility of the measurements is 4 times better.

**Materials.** Water was first deionized by means of ionexchange resins and then doubly distilled. Its conductivity was always less than  $1.0 \times 10^{-6} \Omega^{-1} \cdot \text{cm}^{-1}$ . 2-Propanol (Aldrich HPLC grade) and ethylene glycol monoisopropyl ether (Tokyo Kasei Kogyo Co.) were used without further purification. The claimed purities for the two chemicals were, respectively, 99.5 and more than 99 mass %. All samples were used directly from the manufacturers' bottles, which were kept tightly sealed to minimize, as far as possible, the absorption of atmospheric water and carbon dioxide. The measured properties and those given in the literature are given in Table 1.

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Table 1. Comparison of Densities  $\rho$ , Extensive Properties  $A_p = -(\partial V_m/\partial T)_p$  (Equal to the Product of the Molar Volumes  $V_m$  and the Isobaric Thermal Expansivities  $\alpha_p$ ), Molar Isobaric Heat Capacities  $C_p$ ,<sup>n</sup> and Speeds of Sound *u* of Liquids with the Literature at 298.15 K

	$\varrho/(\mathrm{kg}\mathrm{m}^{-3})$		$A_p/(mm^{3}K^{-1}mol^{-1})$		$C_p/(J\cdot K^{-1}\cdot mol^{-1})$		$u/(\mathbf{m}\cdot\mathbf{s}^{-1})$	
	exptl	lit. <sup>a-f</sup>	exptl	lit. <sup>a,d</sup> g,h	exptl	lit. $^{a,i-k}$	exptl	lit. <sup>c,l,m</sup>
water	_	997.048 <sup>a,n</sup>	-	$4.647^{a,n}$	_	$75.292^{a,n}$	_	$1496.687^{l,n}$ $1497.00^{c}$
2-propanol	-	780.69 <sup>b,n</sup> 780.62 <sup>c</sup> 780.80 <sup>d</sup>	-	83.79 <sup>d,n</sup> 82.37 <sup>g</sup> 81.91 <sup>h</sup>		$161.2^{i,n}$ $154.55^{j}$	1137.07	1138.09° 1134.26 <sup>m</sup>
2-ethylene glycol monoisopropyl ether	-	899.42 <sup>e,n</sup> 899.6 <sup>f</sup>	-	$115.2^{g,n}$	-	$238.8^{k,n}$	1266.27	-

<sup>a</sup> Reference 13. <sup>b</sup> Reference 14. <sup>c</sup> Reference 8. <sup>d</sup> Reference 5. <sup>e</sup> Reference 7. <sup>f</sup> Reference 15. <sup>g</sup> Reference 16. <sup>h</sup> Reference 17. <sup>i</sup> Reference 18. <sup>j</sup> Reference 19. <sup>k</sup> Reference 20. <sup>l</sup> Reference 12. <sup>m</sup> Reference 9. <sup>n</sup> Value chosen for the calculation of the quantities  $K_S$ ,  $K_S^E$ , and  $u^D$ .

Mixtures were prepared by mass at room temperature with a precision of 0.1 mg from freshly thoroughly degassed samples of water and of organic component. They were stored in air-tight bottles. Corrections for buoyancy were included in the calculation of the mole fractions which are believed to be accurate to within 1 part in  $10^4$ .

#### **Results and Discussion**

It proved to be impractical to make ultrasonic speed measurements at the same concentrations as those used previously for density measurements (7, 14). Excess molar volumes  $V_{\rm m}^{\rm E}$  at the mole fractions of the ultrasonic speed measurements were obtained by cubic spline interpolation.

The molar quantity  $K_S = V_m \kappa_S = -(\partial V_m / \partial p)_S$  has no universally acceptable "correct" name, since it is customary to reserve the term "compressibility" for the intensive property  $\kappa_S = V_m^{-1} (\partial V_m / \partial p)_S$ .  $\kappa_S$  and  $K_S$  are calculated from the Newton-Laplace equation

$$\kappa_{\rm S} = (\varrho u^2)^{-1} = V_{\rm m} (M u^2)^{-1} \tag{1}$$

$$K_{\rm S} = V_{\rm m}^{2} (M u^2)^{-1} \tag{2}$$

where  $\rho$  is the density and M the molar mass of the mixture. Equations 1 and 2 are valid, provided that there is a negligible amount of absorption of the acoustic wave. In that case, the ultrasonic speed may be regarded as being a "true" thermodynamic quantity (21).

Defining the ideal quantity  $K_S^{id}$  is not as straightforward as for the ideal molar volume  $V_m^{id}(2)$ . One may write a defining equation in terms of other well-established ideal quantities

$$K_S^{\rm id} = K_T^{\rm id} - T(A_p^{\rm id})^2 / C_p^{\rm id}$$
(3)

where  $K_{\rm T} = -(\partial V_{\rm m}/\partial p)_T$ ,  $A_p = (\partial V_{\rm m}/\partial T)_p$ , and  $C_p$  is the molar isobaric heat capacity (22). The ideal values of all three of these quantities are the mole fraction weighted adducts of the corresponding properties of the pure components.

The corresponding excess molar quantity  $K_S^{\text{E}}$  is calculated from the equation

$$K_S^{\rm E} = K_S - K_S^{\rm id} \tag{4}$$

Uncertainties in the values of  $A_p$  and  $C_p$  for the amphiphilic species lead to uncertainties on the order of  $0.1-0.2 \text{ m}^3 \text{PPa}^{-1}\text{-mol}^{-1}$  at the extrema of  $K_S^{\text{E}}$ . The level of internal consistency is an order of magnitude better.

Insofar as the Newton-Laplace equation is valid, the ultrasonic speed may be expressed solely in terms of thermodynamic quantities

$$u = V_{\rm m} (MK_{\rm s})^{-1/2} \tag{5}$$



**Figure 1.** (a, top) Experimental ultrasonic speeds at 298.15 K for the binary mixtures containing  $(1 - x_2)$  water  $(1) + x_2$  1-propanol (2) [( $\Box$ ) ref 22],  $(1 - x_2)$  water  $(1) + x_2$  2-propanol (2) [( $\bigcirc$ ) this work; (+) ref 9; ( $\diamond$ ) ref 8], and  $(1 - x_2)$  water  $(1) + x_2$  ethylene glycol monoisopropyl ether (2) [( $\oplus$ ) this work]. (b, bottom) Experimental ultrasonic speeds at 298.15 K in the water-rich region for the binary mixtures containing  $(1 - x_2)$  water  $(1) + x_2$  1-propanol (2) [( $\Box$ ) ref 22],  $(1 - x_2)$  water  $(1) + x_2$  2-propanol (2) [( $\Box$ ) ref 22],  $(1 - x_2)$  water  $(1) + x_2$  2-propanol (2) [( $\Box$ ) this work; (+) ref 9; ( $\diamond$ ) ref 8], and  $(1 - x_2)$  water  $(1) + x_2$  ethylene glycol monoisopropyl ether (2) [( $\oplus$ ) this work].

This implies that we can calculate the ultrasonic speed  $u^{id}$  in an "ideal" mixture

$$u^{\rm id} = V_{\rm m}^{\rm id} (MK_S^{\rm id})^{-1/2}$$
 (6)

and its deviation  $u^{\mathrm{D}}$  from the measured values for the same composition such as (1)

$$u^{\rm D} = u - u^{\rm id} \tag{7}$$

The values of  $u, K_S, K_S^E$ , and  $u^D$  are reported in Table 2.

Table 2. Mole Fractions  $x_2$ , Extensive Properties  $K_S = -(\partial V_m/\partial p)_S$ , Excess Molar Quantities  $K_S^E$ , Deviations  $u^D$  from the Ideal Ultrasonic Speed of Water (1) with 2-Propanol (2) and with Ethylene Glycol Monoisopropyl Ether (2) at 298.15 K

	u/	$K_{\mathrm{S}^{a}}$	$K_{S}^{\mathbf{E} a}$	$u^{D/}$
$x_2$	$(m \cdot s^{-1})$	$(m^{3} PPa^{-1} mol^{-1})$	$(m^{3}PPa^{-1}mol^{-1})$	$(m \cdot s^{-1})$
		$W_{otor}(1) \pm 2 Prop($	anol (9)	
0	1406 697	water (1) $\pm 2$ -rropa		٥
0 010 23	1595.88	8.07	-0.82	67.7
0.010.20	1552.31	8.04	-1.60	125.0
0.030.04	1577.40	8.04	-2.38	177.9
0.031.18	1579.81	8.04	-2.47	183.2
0.039 99	1597.93	8.07	-3.12	222.0
0.049 76	1612.69	8.15	-3.78	257.0
0.060 19	1620.85	8.31	-4.42	284.3
0.070 05	1620.00	8.55	-4.92	299.4
0.080 06	1611.80	8.88	-5.34	305.6
0.089 93	1599.19	9.28	-5.69	305.7
0.099 84	1584.51	9.72	-5.99	302.5
0.120 46	1552.76	10.72	-6.52	291.4
0.139 69	1523.00	11.74	-6.92	277.5
0.160 94	1496.35	12.86	-7.35	265.6
0.179 35	1471.80	13.92	-7.63	201.8
0.187 49	1404.34	14.00	-1.19	240.0
0.199.00	1402.24	16.03	-8.41	242.0
0.229 93	1391.08	19.17	-8.86	206.9
0.319.69	1357 24	22.25	-9.24	185.0
0.379 64	1322.77	26.15	-9.48	160.9
0.439 83	1294.40	30.22	-9.51	139.9
0.499 53	1270.58	34.39	-9.36	121.3
0.559 26	1249.86	38.71	-9.02	104.4
0.619 17	1231.50	43.18	-8.51	88.8
$0.679\ 10$	1214.83	47.81	-7.82	74.1
$0.738\ 97$	1199.47	52.58	-6.94	60.1
0.788 84	1187.33	56.71	-6.04	48.8
0.838 76	1175.58	60.98	-4.98	37.7
0.878 69	1156.64	64.03	-4.00	28.8
0.920 43	1147 98	71.89	-1.66	10.4
0.998 33	1137.50	76.09	-0.07	0.4
1	1137.07	76.26	0	0
Wat	tor(1) + F	thylene Glycol Mor	oisopropyl Ether (	(2)
0	1496 687			<i></i>
0.010 03	1537.49	8.05	-0.87	69.5
0.020 29	1572.51	8.06	-1.70	128.8
0.033 28	1604.43	8.19	-2.62	185.8
0.039 88	1614.65	8.32	-3.03	206.8
$0.050\ 01$	1622.29	8.58	-3.58	229.1
0.059 99	1621.48	8.95	-4.01	240.8
0.070 04	1615.03	9.39	-4.37	245.3
0.080 23	1504.40	9.88	-4.68	245.3
0.090.07	15994.49	10.40	-4.55	242.0
0.10002 0.12002	1561 46	12.08	-5.58	229.8
0 140 17	1541 10	13.28	-5.93	219.7
0.160 02	1522.96	14.49	-6.23	209.8
0.180 12	1506.28	15.75	-6.49	200.0
0.200 30	1491.15	17.03	-6.73	190.7
0.22993	1471.26	18.95	-7.02	177.6
$0.270\ 06$	1447.99	21.63	-7.30	161.4
0.319 98	1423.54	25.06	-7.52	143.1
0.379 97	1398.95	29.32	-7.60	123.5
0.440.09	1378.02	30.74	-7.40	20.0
0.559 98	1343.65	43.04	-6.69	75.3
0.570 54	1340.97	43.88	-6.58	72.8
0.620 03	1329.20	47.90	-6.04	61.9
$0.680\ 01$	1316.33	52.83	-5.31	49.6
0.740 04	1304.40	57.85	-4.47	38.1
0.789 98	1295.62	62.08	-3.71	29.5
0.840.67	1287.55	00.40 60.95	-2.80	21.0 15 C
0.920 10	1276 17	73 32	-1.47	10.1
0.960 00	1271.01	76.79	-0.75	4.8
1	1266.27	80.29	0	0

 $a \ 1 \ PPa = 10^{15} \ Pa$ 



**Figure 2.** Excess molar quantities  $K_{\Sigma}^{E}$  at 298.15 K for the binary mixtures containing  $(1 - x_2)$  water  $(1) + x_2$  1-propanol (2) [(---) four-segment model equations applied to data from ref 22],  $(1 - x_2)$  water  $(1) + x_2$  2-propanol (2) [(O) this work; (--) four-segment model equations applied to this work], and  $(1 - x_2)$  water  $(1) + x_2$  ethylene glycol monoisopropyl ether (2) [( $\bullet$ ) this work; (--) four-segment equations applied to this work].

The values of the ultrasonic speeds are presented in Figure 1. Our results for the 2-propanol + water system agree closely in the water-rich region and for the pure solvent with the literature data (8). Some differences are, however, observed in the amphiphile-rich region (9). Figure 1 also shows the ultrasonic speeds of 1-PrOH + water mixtures (23). The ultrasonic speeds for this system and the 2-PrOH + water and ethylene glycol monoisopropyl ether + water mixtures have similar mole fraction dependence profiles. The sharp increase in u with amphiphile content in waterrich mixtures is characteristic of all  $C_m E_n$  + water systems. The well-defined maximum tends to decrease with both increasing alkyl chain length and increasing polar head group size. It is unfortunate that we have been unable to obtain commercially synthesized 2-propoxyethanol.

The shapes of the  $K_S^E$  curves, as shown in Figure 2, are strongly reminiscent of the excess molar volumes. In both cases, the 2-PrOH + water system does not exhibit the same sharp change of slope at  $x_2 = 0.06$  that is characteristic of 1-PrOH + water. Of some interest is the partial excess molar property  $K_S$  of water, defined as

$$K_{S,W}^{E} = K_{S}^{E} - \partial K_{S}^{E} / \partial \alpha_{A}$$
(8)

where  $x_A$  holds for the mole fraction of the amphiphile A. The composition dependence of  $K_{S,W}^{E}$  in the water-rich region is shown in Figure 3a. We see significant changes of slope for all three systems, with that for 1-ProH + water being more pronounced than for the aqueous mixtures of either of the branched species. At amphiphile-rich compositions, as seen in Figure 3b, both of the alkanol + water mixtures show rapid decreases which are clearly not evident for the ethylene glycol monoisopropyl ether + water mixtures (or any other alkoxyethanol + water system).

The changes of slope that have been observed for the excess and the partial excess molar properties of 1-PrOH + water have been observed to a more marked degree for the micelle-forming  $C_6E_n$  + water systems and the "borderline" surfactant  $C_4E_1$  + water (1, 3, 24). The rationale is that, at a critical micelle concentration or its analog, the amphiphile undergoes a significant change in its mode of self-aggregation. 1-Propanol appears to be able to form some type of labile micelle-like clusters more effectively than its isomer.



**Figure 3.** (a, top) Partial excess molar compressibilities  $K_{S,W}^E$  of water at 298.15 K in the water-rich region for the binary mixtures containing  $(1 - x_2)$  water  $(1) + x_2$  1-propanol (2),  $(1 - x_2)$  water  $(1) + x_2$  2-propanol (2), and  $(1 - x_2)$  water  $(1) + x_2$  ethylene glycol monoisopropyl ether (2). Symbols have the same meaning as in Figure 2. (b, bottom) Partial excess molar compressibilities  $K_{S,W}^E$  of water at 298.15 K for the binary mixtures containing  $(1 - x_2)$  water  $(1) + x_2$  1-propanol (2),  $(1 - x_2)$  water  $(1) + x_2$  2-propanol (2),  $(1 - x_2)$  water  $(1) + x_2$  2-propanol (2),  $(1 - x_2)$  water  $(1) + x_2$  2-propanol (2),  $(1 - x_2)$  water  $(1) + x_2$  2-propanol (2),  $(1 - x_2)$  water  $(1) + x_2$  2-propanol (2),  $(1 - x_2)$  water  $(1) + x_2$  ethylene glycol monoisopropyl ether (2). Symbols have the same meaning as in Figure 2.

Table 3. Optimized Four-Segment Model Parameters for the Excess Molar Quantities  $K_S^{\rm E}$  of Water (1) with 1-Propanol (2), with 2-Propanol (2), and with Ethylene Glycol Monoisopropyl Ether (2) at 298.15 K<sup>a</sup>

	1-PrOH	2-PrOH	2-EGMIPE
xA	0.060	0.075	0.052
$x_{\rm B}$	0.225	0.275	0.225
$\boldsymbol{x}_{\mathrm{C}}$	0.725	0.650	0.550
$a_{\rm W}$	-67.6	-79.7	-88.44
$b_{W}$	-38.0	-58.0	240
cw	4105	2707	2533
qw	-2.84	-4.60	-3.78
q <sub>A</sub>	-1.02	-0.59	2.74
$\hat{b}_{ m L}$	-17.9	-27.0	-25.9
$a_{\rm A}$	-30.0	-41.0	-18.4
$b_T$	1.90	4.20	2.90
$10^2\sigma$	0.75	1.75	0.95

<sup>a</sup> Unit of  $K_S^E$  and coefficients: m<sup>3</sup>·PPa<sup>-1</sup>·mol<sup>-1</sup> (1 PPa = 10<sup>15</sup> Pa).

The difference in the shapes of the amphiphile-rich regions of the partial excess molar properties of water for alkanols on the one hand and alkoxyethanols on the other must reflect important differences in the modes of selfaggregation of the pure amphiphiles. In the alkanol case, addition of water has a profound effect upon the presumed cyclic oligomeric structure. In the alkoxyethanol case, it appears that water is incorporated into the amphiphile structure without any significant change in the latter's scheme of self-aggregation.

The calculated values of the molar quantity  $K_S^E$  have been fitted by the most recent set of four-segment model equations (3). These equations are given in the Appendix. This model, as its name implies, involves analyzing the excess molar property data of amphiphile + water systems on the assumption that the total composition range can be treated as being made up of four reasonably discrete regions (segments). The version of the model maintains continuity of  $dQ^E/dx_A$  at each of the three junction segments but derives its fitting capability from allowing discontinuities in  $d^2Q^E/dx_A^2$ . The values of the optimized four-segment model parameters for the three 1-propanol +, 2-propanol +, and ethylene glycol monoisopropyl ether + water systems are summarized in Table 3.

## **Appendix.** Four-Segment Model Equations

Water-Rich Segment.

$$0 \le x_{\rm A} \le x_1$$

$$Q^{\rm E} = a_{\rm W}(x_{\rm A} - x_{\rm A}^{3}) + b_{\rm W}(x_{\rm A}^{2} - x_{\rm A}^{3}) + c_{\rm W}x_{\rm A}^{3}$$
 (a)

where  $Q^E$  represents an excess molar property and  $x_A$  the mole fraction of the amphiphile A.

Pseudolamellar Segment.

$$x_2 \le x_A \le x_3$$
  
 $Q^E = q_W(1 - x_A) + q_A x_A + b_L x_A(1 - x_A)$  (b)

Organic-Rich Segment.

 $x_3 \leq x_A \leq 1$ 

$$\begin{aligned} \boldsymbol{Q}^{\rm E} &= a_{\rm A}(1-x_{\rm A})(1-f_{\rm a})^2 + 3[\boldsymbol{Q}^{\rm E}(x_3)](3f_{\rm a}^{\ 2}-2f_{\rm a}^{\ 3}) + \\ & (1-x_{\rm A})(1-f_{\rm a})^2 \ ({\rm c}) \end{aligned}$$

where

$$f_{a} = (1 - x_{A})/(1 - x_{3})$$
$$[Q^{E}(x_{3})] = q_{W}(1 - x_{3}) + q_{A}x_{3} + b_{L}x_{3}(1 - x_{3})$$
$$\{[dQ^{E}/dx_{A}](x_{3})\} = q_{A} - q_{W} + b_{L}(1 - 2x_{3})$$

Transitional Segment.

$$x_1 \leq x_A \leq x_2$$

$$\begin{split} & Q^{\rm E} = b_T (f_T^{\ 2} - 2f_T^{\ 3} + f_T^{\ 4}) + [Q^{\rm E}(x_1)](4f_T^{\ 3} - 3f_T^{\ 4}) + \\ & [Q^{\rm E}(x_2)](1 - 4f_T^{\ 3} + 3f_T^{\ 4}) + \{[{\rm d}Q^{\rm E}/{\rm d}x_{\rm A}](x_1)\}(x_2 - x_1) \times \\ & (f_T^{\ 3} - f_T^{\ 4}) - \{[{\rm d}Q^{\rm E}/{\rm d}x_{\rm A}](x_2)\}(x_2 - x_1)(f_T^{\ } - f_T^{\ 3} - f_T^{\ 4}) \ ({\rm d}) \} \end{split}$$

where

$$f_T = (x_2 - x_A)/(x_2 - x_1)$$
$$[Q^{\rm E}(x_1)] = a_{\rm W}(x_1 - x_1^3) + b_{\rm W}(x_1^2 - x_1^3) + c_{\rm W}x_1^2$$

$$\{[dQ^{E}/dx_{A}](x_{1})\} = a_{W}(1 - 3x_{1}^{2}) + b_{W}(2x_{1} - 3x_{1}^{2}) + 3c_{W}x_{1}^{2}$$

$$[Q^{E}(x_{2})] = q_{W}(1 - x_{2}) + q_{A}x_{2} + b_{L}x_{2}(1 - x_{2})$$

$$\{[dQ^{L}/dx_{A}](x_{2})\} = q_{A} - q_{W} + b_{L}(1 - 2x_{2})$$

 $a_{\rm w}$  is the apparent excess molar property of the amphiphile A at infinite aqueous dilution.  $b_W$  and  $c_W$  are solute-solute interaction parameters. The former has been associated with hydration cosphere overlap and the latter with solute cluster formation.  $q_{\rm W}$  and  $q_{\rm A}$  are excess molar properties of water and the amphiphile, respectively, in a hypothetical pseudolamellar state.  $b_{\rm L}$  is some type of interface property of that state.  $a_A$  is the apparent excess molar property of water at infinite dilution in the amphiphilic solute.  $b_T$  is a data-fitting parameter related to the range of compositions that are roughly correlated with miscibility gaps.

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